

On Non-Linear Oscillation: an Analytical Series Solution

Mahmoud Bayat¹, Iman Pakar², Amin Barari³, Milad Geraili Nejad⁴, Mostafa Motevalli⁵

¹Young Researchers and Elites club, Science and Research Branch, Islamic Azad University, Tehran, Iran

²Department of Civil Engineering, Mashhad Branch, Islamic Azad University, Mashhad, Iran

³Department of Civil Engineering, Aalborg University, Sohngårdsholmsvej 57, 9000 Aalborg, Aalborg, Denmark

E-mail: amin78404@yahoo.com . ab@civil.aau.dk

⁴Department of Mechanical Engineering, Babol University of Technology, Babol, Iran, P. O. Box 484

⁵Department of Civil Engineering, Azad University, Central Tehran Branch, Tehran, Iran

Abstract: *In this paper, we have applied a new kind of analytical methods called "Homotopy perturbation Method" (HPM) for two basic cases of many complicated cases. We have considered the governing equations of the problems to show the accuracy of the method the achieved results are compared with those from numerical solutions using Runge-Kutta method. It is shown that there is an excellent agreement for the whole domain. Some charts are also presented to have another comparison with energy balance method for different parameters of the problems.*

Keywords: *non-linear oscillation; analytical solution; vibrating system; Homotopy Perturbation Method (HPM)*

1 Introduction

Differential equations are always used to represent many models of dynamical systems in physics and engineering areas. Applied mathematics is an interesting subject of engineers and scientists to prepare better understandings of the engineering problems for a long time. Finding novel techniques to apply and solve

the governing differential equations has been another interesting field in mechanics and mathematics [1, 2].

The equations are complex when we have nonlinear terms in it. It is not possible to apply traditional methods to solve them or prepare an exact solution for them, but it is possible to find approximate analytical solitons to overcome the shortcomings of traditional methods and valid for whole domain of the problem. Recently, considerable attention has been paid on approximate methods such as: Homotopy Perturbation method [3-6], Energy Balance [7-13], Harmonic Balance [14], Homotopy Analysis Method [15, 16] Variational Iteration Method [17-20], Max-Min [21-25], Differential Transform [26], Amplitude Frequency Formulation [27-28] and Adomian Decomposition [29], Hamiltonian approach [30], Variational approach [31].

This paper considers the following general nonlinear oscillators:

$$u'' + \omega_0^2 u + \mathcal{F}(u) = 0 \quad (1)$$

With initial conditions:

$$u(0) = A, \quad u'(0) = 0 \quad (2)$$

where f is a nonlinear function of u , u' , u in this preliminary report, we suppose the simplest case, i.e., f depends upon only the function of u . If there is no small parameter in the equation, traditional perturbation methods cannot be applied directly. Recently, considerable attention has been paid to the analytical solutions for nonlinear equations without possible small parameters. Traditional perturbation methods have many shortcomings, and they are not valid for strongly nonlinear equations. Mechanical oscillatory systems are often governed by nonlinear differential equations. It is well known that a nonlinear equation of this type is often linearized by retaining the first term of the Taylor series expansion of the restoring force in a neighborhood of the equilibrium point. This procedure yields acceptable results for many cases, but is unable to show the amplitude dependence of the oscillation period.

2 Overview of the Analytical Method

To explain the basic idea of the HPM for solving nonlinear differential equations we consider the following nonlinear differential equation:

$$A(u) - f(r) = 0, \quad r \in \Omega \quad (3)$$

Subject to boundary condition

$$B(u, \partial u / \partial n) = 0, \quad r \in \Gamma \quad (4)$$

where A is a general differential operator, B a boundary operator, $f(r)$ is a known analytical function, Γ is the boundary of domain Ω and $\partial u/\partial n$ denotes differentiation along the normal drawn outwards from Ω . The operator A can, generally speaking, be divided into two parts: a linear part L and a nonlinear part N . Equation (3) therefore can be rewritten as follows:

$$L(u) + N(u) - f(r) = 0 \quad (5)$$

In case that the nonlinear equation (3) has no “small parameter”, we can construct the following Homotopy:

$$H(v, p) = L(v) - L(u_0) + pL(u_0) + p(N(v) - f(r)) = 0 \quad (6)$$

Where,

$$v(r, p): \Omega \times [0, 1] \rightarrow R \quad (7)$$

In equation (9), $p \in [0, 1]$ is an embedding parameter and u_0 is the first approximation that satisfies the boundary condition. We can assume that the solution of equation (6) can be written as a power series in p , as following:

$$v = v_0 + pv_1 + p^2v_2 + \dots, \quad (8)$$

And the best approximation for solution is:

$$u = \lim_{p \rightarrow 1} v = v_0 + v_1 + v_2 + \dots, \quad (9)$$

When, Eq. (6) correspond to equation (3) and equation (9) becomes the approximate solution of equation (3).

3 Description of the First Case

In this section we consider a rigid frame (Fig. 1) which is forced to rotate at the fixed rate Ω . While the frame rotates, the simple pendulum oscillates.

The governing equation is:

$$\ddot{\theta} + (1 - \beta \cos \theta) \sin \theta = 0, \quad \theta(0) = A, \quad \dot{\theta}(0) = 0 \quad (10)$$

Where

$$\beta = \frac{\Omega^2 r}{g} < 1$$

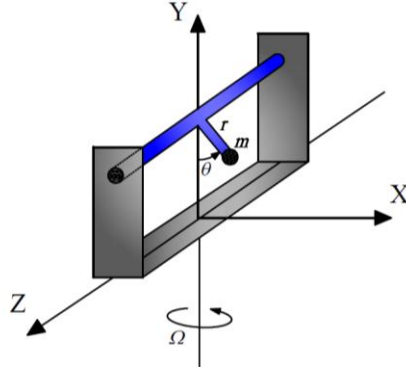


Figure 1

Rotating frame connected to a pendulum

3.1 Application of Homotopy Perturbation Method

We use Taylor series instead of functions of $\sin(\theta(t))$ and $\cos(\theta(t))$:

$$\sin(\theta) = \theta - \frac{1}{6}\theta^3 \quad (11)$$

$$\cos(\theta) = 1 - \frac{1}{2}\theta^2 \quad (12)$$

We substitute equations (11), (12) in equation (10), so:

$$\ddot{\theta} + \left(1 - \beta \left(1 - \frac{\theta^2}{2}\right)\right) \left(\theta - \frac{\theta^3}{6}\right) \quad (13)$$

Separate the linear and nonlinear part:

$$L : \ddot{\theta} + \theta - \beta\theta \quad (14)$$

$$N : \ddot{\theta} + \theta - \beta\theta - \frac{1}{6}\theta^3 + \frac{2}{3}\beta\theta^3 - \frac{1}{12}\beta\theta^5 \quad (15)$$

Now we form the Homotopy as follows:

$$H(\theta, p) = (1-p)(\ddot{\theta} + \theta - \beta\theta) + p \left(\ddot{\theta} + \theta - \beta\theta - \frac{\theta^3}{6} + \frac{2}{3}\beta\theta^3 - \frac{1}{12}\beta\theta^5 \right) \quad (16)$$

$$\theta(t) = \theta_0 + p\theta_1 \quad (17)$$

By substituting equation (17) in equation (16):

$$\begin{aligned}
 H(\theta, p) &= (1-p) \left[\ddot{\theta}_0 + p\ddot{\theta}_1 + \theta_0 + p\theta_1 - \beta(\theta_0 + p\theta_1) \right] \\
 &+ p \left[\ddot{\theta}_0 + p\ddot{\theta}_1 + \theta_0 + p\theta_1 - \frac{1}{6}(\theta_0 + p\theta_1)^3 - \beta(\theta_0 + p\theta_1) \right. \\
 &\quad \left. + \frac{2}{3}\beta(\theta_0 + p\theta_1)^3 - \frac{1}{12}\beta(\theta_0 + p\theta_1)^5 \right]
 \end{aligned} \tag{18}$$

We simplified equation (18) on the basis of p powers:

$$\begin{aligned}
 H(\theta, p) &= -\frac{1}{12}\beta\theta_1^3 p^6 - \frac{5}{12}\beta\theta_0\theta_1^4 p^5 + \\
 &\left[-\frac{1}{6}\theta_1^3 + \frac{2}{3}\beta\theta_1^3 - \frac{5}{6}\beta\theta_0^2\theta_1^3 \right] p^4 + \left[2\beta\theta_0\theta_1^2 - \frac{5}{6}\beta\theta_0^3\theta_1^2 - \frac{1}{2}\theta_0\theta_1^2 \right] p^3 + \\
 &\left[-\frac{1}{2}\theta_0^2\theta_1 - \frac{5}{12}\beta\theta_0^4\theta_1 + 2\beta\theta_0^2\theta_1 \right] p^2 + \left[\theta_1 - \frac{1}{12}\beta\theta_0^5 + \frac{2}{3}\beta\theta_0^3 - \frac{1}{6}\theta_0^3 + \theta_1'' - \beta\theta_1 \right] p + \\
 &\theta_0 + \theta_0'' - \beta\theta_0
 \end{aligned} \tag{19}$$

Now we should solve these equations:

$$p^0: \ddot{\theta}_0 + \theta_0 - \beta\theta_0 \quad \theta_0(0) = A, \quad \dot{\theta}_0(0) = 0 \tag{20}$$

So:

$$\theta_0(t) = A \cos(\sqrt{1-\beta}t) \tag{21}$$

And

$$\begin{aligned}
 p^1: \ddot{\theta}_1 + \theta_1 - \beta\theta_1 - \frac{1}{12}\beta A^5 \cos(\sqrt{1-\beta}t)^5 + \\
 \frac{2}{3}\beta A^3 \cos(\sqrt{1-\beta}t)^3 - \frac{1}{6}A^3 \cos(\sqrt{1-\beta}t)^3 \quad \theta_1(0) = 0, \quad \dot{\theta}_1(0) = 0
 \end{aligned} \tag{22}$$

So:

$$\begin{aligned}
 \theta_1(t) &= \frac{1}{72} \frac{\cos(\sqrt{1-\beta}t)(\beta A^2 - 12\beta + 3)A^3}{\beta - 1} \\
 &- \frac{1}{4608\beta - 4608} \left[120A^3 \left(\left(-\frac{1}{8}\beta A^2 + \frac{4}{5}\beta - \frac{1}{5} \right) \cos(3\sqrt{1-\beta}t) - \frac{1}{120}\beta A^2 \cos(5\sqrt{1-\beta}t) + \right. \right. \\
 &\left. \left. \left(\frac{2}{3}\beta A^2 - \frac{36}{5}\beta + \frac{9}{5} \right) \cos(\sqrt{1-\beta}t) + \sqrt{1-\beta} \left(\beta A^2 - \frac{48}{5} + \beta \frac{12}{5} \right) \sin(\sqrt{1-\beta}t) \right) \right]
 \end{aligned} \tag{23}$$

As seen before in equation (17) we have:

$$\begin{aligned}
 \theta_{HPM} &= A \cos(\sqrt{1-\beta}t) + \frac{1}{72} \frac{\cos(\sqrt{1-\beta}t)(\beta A^2 - 12\beta + 3)A^3}{\beta - 1} \\
 &- \frac{1}{4608\beta - 4608} \left[120A^3 \left(\left(-\frac{1}{8}\beta A^2 + \frac{4}{5}\beta - \frac{1}{5} \right) \cos(3\sqrt{1-\beta}t) - \frac{1}{120}\beta A^2 \cos(5\sqrt{1-\beta}t) + \right. \right. \\
 &\left. \left. \left(\frac{2}{3}\beta A^2 - \frac{36}{5}\beta + \frac{9}{5} \right) \cos(\sqrt{1-\beta}t) + \sqrt{1-\beta} \left(\beta A^2 - \frac{48}{5} + \beta \frac{12}{5} \right) \sin(\sqrt{1-\beta}t) \right) \right]
 \end{aligned} \tag{24}$$

3.2 Results and Discussions

To show the accuracy of the results, the HPM solutions are compared with the numerical ones. Table 1 represents the comparison of HPM and Runge-Kutta for different values.

A brief discussion of the numerical method used in this paper is described in Appendix A. Then, we have compared the results with those obtained by EBM solution, in Figs. 2 and 3:

$$\omega_{EBM} = A \cos\left(\frac{2}{A} \sqrt{\cos\left(\frac{\sqrt{2}}{2}A\right) - \cos A + \frac{\beta}{2}(\cos^2 A - \cos^2\left(\frac{\sqrt{2}}{2}A\right))} \times t\right) \tag{25}$$

As it is evident, a same manner with a high accuracy is gained by HPM. The EBM is shortly explained in Appendix B.

For table 1

Case 1: $g = 10, r = 2, \Omega = 1, A = \pi/12$

Case 2: $g = 10, r = 0.5, \Omega = 2.5, A = \pi/4$

Table 1
The results of HPM and numerical solution for $\theta(t)$

T	Case 1			Case 2		
	HPM	Numerical solution	Error	HPM	Numerical solution	Error
0	0.2618	0.2618	0.0000	0.7854	0.7854	0.0000
0.4	0.2428	0.2453	0.0099	0.7448	0.7416	0.0043
0.8	0.1958	0.1978	0.0099	0.6180	0.6153	0.0043
1.2	0.1240	0.1252	0.0099	0.4225	0.4207	0.0043
1.6	0.0365	0.0369	0.0098	0.1806	0.1798	0.0042
2	-0.0556	-0.0562	0.0100	-0.0811	-0.0807	0.0049
2.4	-0.1407	-0.1421	0.0100	-0.3340	-0.3325	0.0045
2.8	-0.2079	-0.2100	0.0099	-0.5502	-0.5477	0.0045
3.2	-0.2489	-0.2514	0.0099	-0.7056	-0.7024	0.0046
3.6	-0.2585	-0.2611	0.0099	-0.7826	-0.7789	0.0047
4	-0.2354	-0.2377	0.0099	-0.7724	-0.7687	0.0048
4.4	-0.1826	-0.1844	0.0098	-0.6761	-0.6728	0.0050
4.8	-0.1067	-0.1077	0.0098	-0.5047	-0.5021	0.0050
5.2	-0.0172	-0.0174	0.0092	-0.2774	-0.2761	0.0050
5.6	0.0744	0.0751	0.0101	-0.0197	-0.0197	0.0004
6	0.1565	0.1581	0.0100	0.2401	0.2388	0.0057
6.4	0.2189	0.2211	0.0099	0.4737	0.4711	0.0055
6.8	0.2536	0.2562	0.0099	0.6552	0.6515	0.0056

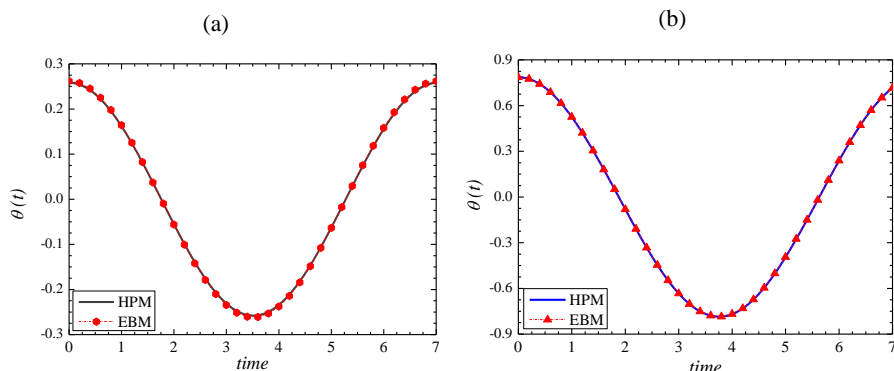


Figure 2

Comparison of time history response of HPM solution with the EBM solution for

(a) $g = 10, r = 2, \Omega = 1, A = \pi/12$, (b) $g = 10, r = 0.5, \Omega = 2.5, A = \pi/4$

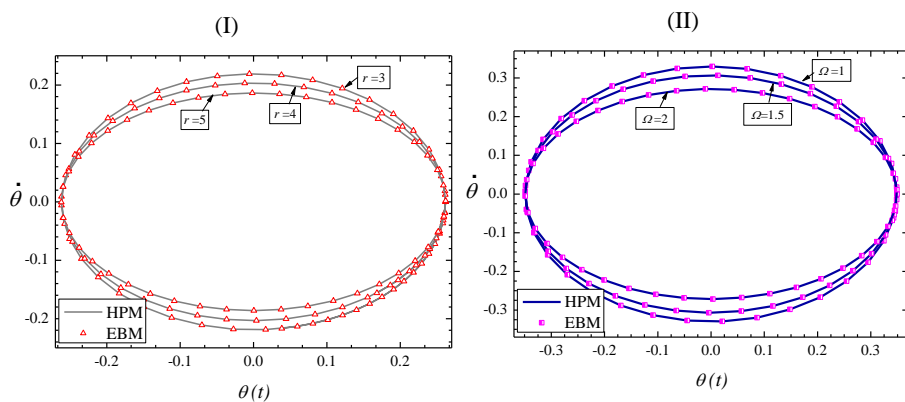


Figure 3

Comparison of phase plan of HPM solution with EBM solution for variation parameter

(I) $g = 10, r = 2, A = \pi/12$, (II) $g = 10, \Omega = 1, A = \pi/9$

4 Description of the Second Problem

We first consider the following nonlinear oscillator (Fig. 4):

$$(1 + Ru^2)\ddot{u} + Ru\dot{u}^2 + \omega_0^2 u + \frac{1}{2} \frac{R g u^3}{l} = 0 \quad u(0) = A, \dot{u}(0) = 0 \quad (26)$$

where

$$\omega_0^2 = \frac{k}{m_1} + \frac{Rg}{l}, \quad R = \frac{m_2}{m_1}, \quad \left| u = \frac{x}{l} \right| \ll 1 \quad (27)$$

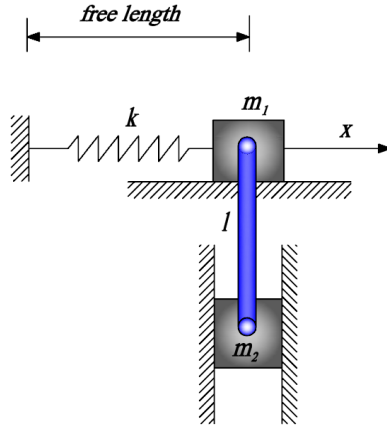


Figure 4
Geometry of Example 2

4.1 Implementation of Homotopy Perturbation Method

The governing equation is:

$$(1 + Ru^2)\ddot{u} + Ru\dot{u}^2 + \omega_0^2 u + \frac{1}{2} \frac{Rg}{l} u^3 \quad (28)$$

Separate the linear and nonlinear part:

$$L : \ddot{u} + \omega_0^2 u \quad (29)$$

$$N : (1 + Ru^2)\ddot{u} + Ru\dot{u}^2 + \omega_0^2 u + \frac{1}{2} \frac{Rg}{l} u^3 \quad (30)$$

Then we create the Homotopy Perturbation:

$$H(u, p) = (1 - p) \left[\ddot{u} + \omega_0^2 u \right] + p \left[(1 + Ru^2)\ddot{u} + Ru\dot{u}^2 + \omega_0^2 u + \frac{1}{2} \frac{Rg}{l} u^3 \right] \quad (31)$$

$$u(t) = u_0 + pu_1 \quad (32)$$

Substitute equation (32) in equation (31), we have:

$$\begin{aligned}
 H(u, p) = & (1-p) [\ddot{u}_0 + p\ddot{u}_1 + \omega_0^2(u_0 + pu_1)] + \\
 & p \left[(1 + R(u_0 + pu_1)^2) (\ddot{u}_0 + p\ddot{u}_1) + R(u_0 + pu_1)(\dot{u}_0 + p\dot{u}_1)^2 \right. \\
 & \left. + \omega_0^2(u_0 + pu_1) + \frac{1}{2} \frac{Rg(u_0 + pu_1)^3}{l} \right]
 \end{aligned} \tag{33}$$

We simplified equation (33) on the basis of p powers:

$$\begin{aligned}
 H(u, p) = & \left[\frac{1}{2} \frac{Rgu_1^3}{l} + Ru_1^2\ddot{u}_1 + Ru_1\dot{u}_1^2 \right] p^4 \\
 & + \left[Ru_1^2\ddot{u}_0 + Ru_0\dot{u}_1^2 + \frac{3}{2} \frac{Rgu_0u_1^2}{l} + 2Ru_1\dot{u}_1\dot{u}_0 + 2Ru_0u_1\ddot{u}_1 \right] p^3 \\
 & + \left[Ru_0^2\ddot{u}_1 + \frac{3}{2} \frac{Rgu_0^2u_1}{l} + Ru_0\dot{u}_0^2 + 2Ru_0\dot{u}_1\dot{u}_1 + 2Ru_0\mu\ddot{u}_0 \right] p^2 \\
 & + \left[\ddot{u}_1 + Ru_0\dot{u}_0^2 + Ru_0^2\ddot{u}_0 + \omega_0^2u_1 + \frac{1}{2} \frac{Rgu_0^3}{l} \right] p + \ddot{u}_0 + \omega_0^2u_0
 \end{aligned} \tag{34}$$

Now we should solve these equations:

$$p^0: \ddot{u}_0 + \omega_0^2u_0 \quad u_0(0) = A, \quad \dot{u}_0(0) = 0 \tag{35}$$

So:

$$u_0(t) = A \cos(\omega_0 t) \tag{36}$$

And

$$p^1: \ddot{u}_1 + Ru_0\dot{u}_0^2 + Ru_0^2\ddot{u}_0 + \omega_0^2u_1 + \frac{1}{2} \frac{Rgu_0^3}{l} \quad u_1(0) = 0, \quad \dot{u}_1(0) = 0 \tag{37}$$

We substitute equation (36) in equation (37) and solve it with the given boundary conditions:

$$\begin{aligned}
 u_1(t) = & -\frac{1}{64} \frac{A^3 Rg \cos(\omega_0 t)}{\omega_0^2 l} + \frac{1}{4} A^3 R \cos(\omega_0 t) + \frac{1}{64} A^3 Rg \cos(3\omega_0 t) \\
 & - \frac{3}{16} \frac{A^3 Rg \omega_0 \sin(\omega_0 t)t}{\omega_0^2 l} - \frac{1}{16} A^3 R \cos(3\omega_0 t) + \frac{1}{4} A^3 R \sin(\omega_0 t)t
 \end{aligned} \tag{38}$$

As seen before in equation (32) we have:

$$\begin{aligned}
 u_{HPM} = & A \cos(\omega_0 t) - \frac{1}{64} \frac{A^3 Rg \cos(\omega_0 t)}{\omega_0^2 l} + \frac{1}{4} A^3 R \cos(\omega_0 t) + \frac{1}{64} A^3 Rg \cos(3\omega_0 t) \\
 & - \frac{3}{16} \frac{A^3 Rg \omega_0 \sin(\omega_0 t)t}{\omega_0^2 l} - \frac{1}{16} A^3 R \cos(3\omega_0 t) + \frac{1}{4} A^3 R \sin(\omega_0 t)t
 \end{aligned} \tag{39}$$

4.2 Results and Ddiscussions

In this part, the results are compared with numerical solutions. The accuracy of the method is shown in Table 2. Figs. 5 and 6 represent the comparison of the HPM and EBM results.

$$u_{EBM} = A \cos \left(\sqrt{\frac{\frac{1}{4}\omega_0^2 A^2 + \frac{3Rg}{32l} A^4}{\frac{1}{4}A^2 + \frac{1}{8}A^4}} \times t \right) \quad (40)$$

For Table 2

Case 1: $g = 10, m_1 = 4, m_2 = 2, l = 1, k = 20, \tan(\pi/6)$

Table 2
The results of HPM and numerical solution for $u(t)$

T	Case 1			Case 2		
	HPM	Numerical solution	Error	HPM	Numerical solution	Error
0	0.5774	0.5774	0.0000	0.8038	0.803848	0.0000
0.05	0.5155	0.5167	0.0024	0.6785	0.677134	0.0020
0.1	0.3376	0.3396	0.0061	0.3268	0.325309	0.0047
0.15	0.0745	0.0758	0.0168	-0.1450	-0.14584	0.0059
0.2	-0.2089	-0.2079	0.0050	-0.5614	-0.56223	0.0014
0.25	-0.4368	-0.4360	0.0019	-0.7859	-0.7841	0.0023
0.3	-0.5607	-0.5626	0.0034	-0.7646	-0.75656	0.0106
0.35	-0.5628	-0.5707	0.0138	-0.4937	-0.48546	0.0170
0.4	-0.4429	-0.4535	0.0235	-0.0452	-0.04258	0.0608
0.45	-0.2179	-0.2243	0.0288	0.4171	0.416369	0.0018
0.5	0.0648	0.0632	0.0260	0.7325	0.725416	0.0097
0.55	0.3298	0.3311	0.0038	0.8168	0.797864	0.0238
0.6	0.5113	0.5188	0.0145	0.6395	0.618087	0.0346
0.65	0.5773	0.5960	0.0314	0.2365	0.228363	0.0356
0.7	0.5196	0.5452	0.0471	-0.2504	-0.24637	0.0163
0.75	0.3452	0.3638	0.0512	-0.6450	-0.6296	0.0245
0.8	0.0842	0.0888	0.0520	-0.8335	-0.79984	0.0421
0.85	-0.1999	-0.2055	0.0276	-0.7588	-0.71746	0.0577
0.9	-0.4306	-0.4471	0.0369	-0.4218	-0.40031	0.0537
0.95	-0.5585	-0.5917	0.0562	0.0668	0.061481	0.0861
1	-0.5648	-0.6113	0.0762	0.5260	0.500082	0.0519

Case 2: $g = 10, m_1 = 5, m_2 = 1, l = 1, k = 50, A = 3 \tan(\pi/12)$

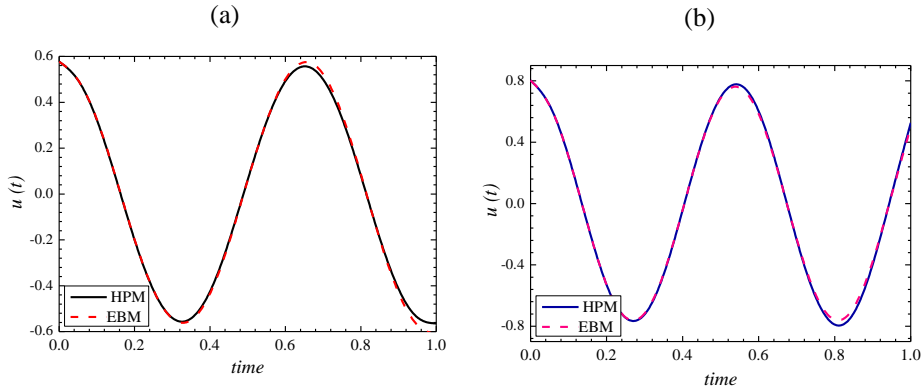


Figure 5

Comparison of time history response of HPM solution with the EBM solution for

(a) $g = 10, m_1 = 4, m_2 = 2, l = 1, k = 20, \tan(\pi/6)$,

(b) $g = 10, m_1 = 5, m_2 = 1, l = 1, k = 50, A = 3 \tan(\pi/12)$

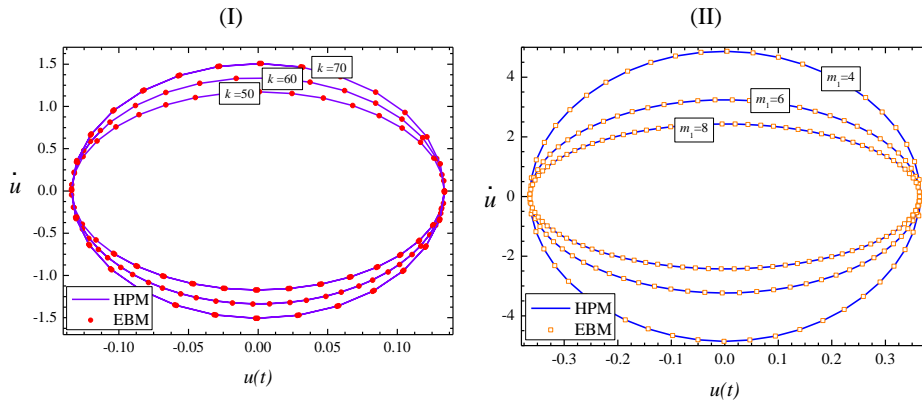


Figure 6

Comparison of phase plan of HPM solution with EBM solution for variation parameter

(I): $g = 10, m_1 = 8, m_2 = 2, l = 1, A = 0.5 \tan(\pi/12)$,

(II): $g = 10, m_2 = 2, l = 1.5, k = 40, A = \tan(\pi/9)$

Conclusion

In this paper Homotopy Perturbation Method was used to solve some practical non-linear equation of oscillators. It was observed that the results obtained by HPM are in very good agreement with those achieved by numerical solution and

another analytical technique namely EBM. It is an advantageous to solve oscillation systems as such problems frequently arise in many branches of sciences and engineering while HPM is much simpler in comparison with other methods. Besides, the exact expression obtained here can be used in a wide range of future numerical or analytical investigations. Following the successful application of the method introduced here for highly non-linear oscillators, HPM is strongly proposed by the authors in exploring solutions to the same problems.

Appendix A. DESCRIPTION OF RK4

The Runge-Kutta method is an important iterative method for the approximation solutions of ordinary differential equations. These methods were developed by the German mathematician Runge and Kutta around 1900. For simplicity, we explain one of the important methods of Runge-Kutta methods, called forth-order Runge-Kutta method.

Consider an initial value problem be specified as follows:

$$y' = f(t, y), \quad y(t_0) = y_0 \quad (\text{A. 1})$$

Then RK4 method is given for this problem as below:

$$y_{n+1} = y_n + \frac{1}{6}h(k_1 + 2k_2 + 2k_3 + k_4),$$

$$t_{n+1} = t_n + h. \quad (\text{A. 2})$$

Where y_{n+1} is the RK4 approximation of $y(t_{n+1})$ and

$$k_1 = f(t_n, y_n),$$

$$k_2 = f\left(t_n + \frac{1}{2}h, y_n + \frac{1}{2}hk_1\right),$$

$$k_3 = f\left(t_n + \frac{1}{2}h, y_n + \frac{1}{2}hk_3\right),$$

$$k_4 = f(t_n + h, y_n + hk_3). \quad (\text{A. 3})$$

Appendix B. An Introduction to Energy Balance Method

Consider a general nonlinear oscillator in the form:

$$u'' + f(u(t)) = 0 \quad (\text{B.1})$$

in which u and t are generalized dimensionless displacement and time variables, respectively. Its variational principle can be easily obtained:

$$J(u) = \int_0^t \left(-\frac{1}{2}u'^2 + F(u) \right) dt \quad (\text{B.2})$$

Where $T = \frac{2\pi}{\omega}$ is period of the nonlinear oscillator, $F(u) = \int f(u)du$.

Its Hamiltonian, therefore, can be written in the form:

$$H = \frac{1}{2}u'^2 + F(u) + F(A) \quad (\text{B.3})$$

$$R(t) = \frac{1}{2}u'^2 + F(u) - F(A) = 0 \quad (\text{B.4})$$

Oscillatory systems contain two important physical parameters, i.e., the frequency ω and the amplitude of oscillation, A . So let us consider such initial conditions:

$$u(0) = 0, \quad u'(0) = 0 \quad (\text{B.5})$$

We use the following trial function to determine the angular frequency ω :

$$u(t) = A \cos(\omega t) \quad (\text{B.6})$$

Substituting (B.6) into u term of (B.4), yield:

$$R(t) = \frac{1}{2}\omega^2 A^2 \sin^2 \omega t + F(A \cos \omega t) - F(A) = 0 \quad (\text{B.7})$$

If, by chance, the exact solution had been chosen as the trial function, then it would be possible to make R zero for all values of t by appropriate choice of ω .

Collocation at $\omega t = \frac{\pi}{4}$ gives:

$$\omega = \sqrt{\frac{2(F(A) - F(A \cos \omega t))}{A^2 \sin^2 \omega t}} \quad (\text{B.8})$$

$$T = \frac{2\pi}{\sqrt{\frac{2(F(A) - F(A \cos \omega t))}{A^2 \sin^2 \omega t}}} \quad (\text{B.9})$$

References

- [1] Dunning, A. G., Tolou, N., Herder, J. L., "Review Article: Inventory of Platforms Towards the Design of a Statically Balanced Six Degrees of Freedom Compliant Precision Stage", *Mechanical Sciences*, 2011, Vol. 2, No. 2, pp. 139-146

- [2] Žilková, J., Timko, J., Girovský, P., “Nonlinear System Control Using Neural Networks”, *Acta Polytechnica Hungarica*, 2006, Vol. 3, No. 4, pp. 85-94
- [3] He, J. H., “Homotopy Perturbation Method for Solving Boundary Value Problems”, *Phys Lett A*, 2006, Vol. 350, No. 1-2, pp. 87-88
- [4] Bayat, M., Pakar, I., Domairry, G., “Recent Developments of Some Asymptotic Methods and Their Applications for Nonlinear Vibration Equations in Engineering Problems: A Review”, *Latin American Journal of Solids and Structures*, 2012, Vol. 9, No. 2, pp. 145-234
- [5] Barari, A., Omidvar, M., Ghotbi, Abdoul R., Ganji, D. D., “Application of Homotopy Perturbation Method and Variational Iteration Method to Nonlinear Oscillator Differential Equations”, *Acta Applicanda Mathematicae*, 2008, Vol. 104, No. 2, pp. 161-171
- [6] Sfahani, M. G., Ganji, S. S., Barari, A., Mirgolbabaie, H., Domairry, G., “Analytical Solutions to Nonlinear Conservative Oscillator with Fifth-Order Non-linearity”, *Earthquake Engineering and Engineering Vibration*, 2010, Vol. 9, No. 3, pp. 367-374
- [7] Bayat, M., Pakar, I., “Application of He’s Energy Balance Method for Nonlinear Vibration of Thin Circular Sector Cylinder”, *Int. J. Phy. Sci.*, 2011, Vol. 6, No. 23, pp. 5564-5570
- [8] Sfahani, M. G., Barari, A., Omidvar, M., Ganji, S. S., Domairry, G., “Dynamic Response of Inextensible Beams by Improved Energy Balance Method”, *Proceedings of the Institution of Mechanical Engineers, Part K: Journal of Multi-body Dynamics*, Vol. 225, No. 1, pp. 66-73
- [9] Barari, A., Kaliji, H. D., Ghadim, M., Domairry, G., “Non-linear Vibration of Euler-Bernoulli Beams”, *Latin American Journal of Solids and Structures*, 2011, Vol. 8, No. 2, pp. 139-148
- [10] Bayat, M., Barari, A., Shahidi, M., “Dynamic Response of Axially Loaded Euler-Bernoulli Beams”, *Mechanika*, 2011, Vol. 17, No. 2, pp. 172-177
- [11] Momeni, M., Jamshidi, N., Barari, A., Ganji, D. D., “Application of He’s Energy Balance Method to Duffing Harmonic Oscillators”, *International Journal of Computer Mathematics*, 2011, Vol. 88, No. 1, 135-144
- [12] Bayat, M., Shahidi, M., Barari, A., Domairry, G., “Analytical Evaluation of the Nonlinear Vibration of Coupled Oscillator Systems”, *Zeitschrift Fur Naturforschung - Section A Journal of Physical Sciences*, 2011, Vol. 66, No. 1-2, pp. 67-74
- [13] Pakar, I., Bayat, M., “Analytical Solution for Strongly Nonlinear Oscillation Systems using Energy Balance Method”, *Int. J. Phy. Sci.*, Vol. 6, No. 22, pp. 5166-5170

-
- [14] Hu, H., Tang, J. H., “Solution of a Duffing-harmonic Oscillator by the Method of Harmonic Balance”, *Journal of Sound and Vibration*, 2006, Vol. 294, No. 3, pp. 637-639
- [15] Ghotbi, A. R., Omidvar, M., Barari, A., “Infiltration in Unsaturated Soils – An Analytical Approach”, *Computers and Geotechnics*, 2011, Vol. 38, No. 6, pp. 777-782
- [16] Ghasemi, E., Soleimani, S., Barari, A., Bararnia, H., Domairry, G., “The Influence of Uniform Suction/Injection on Heat Transfer of MHD Hiemenz Flow in Porous Media”, *Engineering Mechanics*, ASCE, 2012, Vol. 138, No. 1, pp. 82-88
- [17] Miansari, Mo., Miansari, Me., Barari, A., Domairry, G., “Analysis of Blasius Equation for Flat-Plate Flow with Infinite Boundary Value”, *International Journal for Computational Methods in Engineering Science and Mechanics*, 2010, Vol. 11, No. 2, pp. 79-84
- [18] Fouladi, F., Hosseinzadeh, E., Barari, A., Domairry, G., “Highly Nonlinear Temperature Dependent Fin Analysis by Variational Iteration Method”, *Journal of Heat Transfer Research*, Vol. 41, No. 2, pp. 155-165
- [19] Ghotbi, A. R., Barari, A., Omidvar, M., Domairry, G., “Application of Homotopy Perturbation and Variational Iteration Methods to SIR Epidemic Model”, *Journal of Mechanics in Medicine and Biology*, 2011, Vol. 11, No. 1, pp. 149-161
- [20] Omidvar, M., Barari, A., Momeni, M., Ganji, D. D., “New Class of Solutions for Water Infiltration Problems in Unsaturated Soils”, *International Journal of Geomechanics and Geoenvironment*, 2010, Vol. 5, No. 2, pp. 127-135
- [21] Ibsen, L. B., Barari, A., Kimiaieifar, A., “Analysis of Highly Nonlinear Oscillation Systems Using He’s Max-Min Method and Comparison with Homotopy Analysis and Energy Balance Methods”, *Sadhana*, 2010, Vol. 35, No. 4, 1-16
- [22] Ganji, S. S., Barari, A., Ganji, D. D., “Approximate Analysis of Two Mass-Spring Systems and Buckling of a Column”, *Computers & Mathematics with Applications*, 2011, Vol. 61, No. 4, pp. 1088-1095
- [23] Pakar, I., Bayat, M., “An Analytical Study of Nonlinear Vibrations of Buckled Euler-Bernoulli Beams”, *Acta Physica Polonica A*, 2013, Vol. 123, No. 1, pp. 48-52
- [24] Bayat, M., Pakar, I., Shahidi, M., “Analysis of Nonlinear Vibration of Coupled Systems with Cubic Nonlinearity”, *Mechanika*, 2011, Vol. 17, No. 6, pp. 620-629

- [25] Ghadimi, M., Kaliji, H. D., Barari, A., “Analytical Solutions to Nonlinear Mechanical Oscillation Problems”, *Journal of Vibroengineering*, 2011, Vol. 13, pp. 133-144
- [26] Ganji, S. S., Barari, A., Ibsen, L. B., Domairry, G., “Differential Transform Method for Mathematical Modeling of Jamming Transition Problem in Traffic Congestion Flow”, *Central European Journal of Operations Research*, 2012, Vol. 20, No. 1, pp. 87-100
- [27] Fereidoon, A., Ghadimi, M., Barari, A., Kaliji, H. D., Domairry, G., “Nonlinear Vibration of Oscillation Systems using Frequency-Amplitude Formulation”, *Shock and Vibration*, 2012, Vol. 19, No. 3, 323-332
- [28] Pakar, I., Bayat, M., “Vibration Analysis of High Nonlinear Oscillators using Accurate Approximate Methods”, *Structural Engineering and Mechanics*, 2013, Vol. 46, No. 1, pp. 137-151
- [29] Mirgolbabaie, H., Barari, A., Ibsen, L. B., Sfahani, M. G., “Numerical Solution of Boundary Layer Flow and Convection Heat Transfer Over a Flat Plate”, *Archives of Civil and Mechanical Engineering*, 2010, Vol. 10, No. 2, pp. 41-51
- [30] Bayat, M., Pakar, I., Bayat, M., “On the Large Amplitude Free Vibrations of Axially Loaded Euler-Bernoulli Beams”, *Steel and Composite Structures*, 2013, Vol. 14, No. 1, pp. 73-83
- [31] Bayat, M., Pakar, I., “On the Approximate Analytical Solution to Non-Linear Oscillation Systems”, *Shock and Vibration*, 2013, Vol. 20, No. 1, pp. 43-52